

ZERO-DIMENSIONAL STEADY STATE PLASMA
SIMULATION COMPUTER CODE

by

J. C. Sprott

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This note describes a computer code (ZEDTID) that calculates the spatially averaged electron (and ion) density, neutral density, electron temperature, and ion temperature in a steady state cylindrical plasma. It is a simplification of a time-dependent code (SIMULT) described in PLP 505 and is much faster, more accurate, and quite adequate for a variety of quasi-steady state situations such as a cw microwave plasma in a toroidal octupole. It uses a UW library subroutine (ZRNEQ) that seeks a solution of N simultaneous non-linear algebraic equations in N unknowns. In this case, it is used to solve particle balance equations for electrons (or ions) and neutrals and energy balance equations for electrons and ions. The various particle and energy loss terms are a refined version of those presented in PLP 505 and will be described in detail in a forthcoming PLP by Patau. The physical processes considered are listed below:

1. ionization
2. classical radial diffusion (e-i and e-n collisions)
3. obstacle losses
4. microwave heating (including finite cavity Q)
5. electron-ion energy equipartition
6. neutral collisions (excitation)
7. bremsstrahlung
8. synchrotron radiation (ignoring reabsorption)
9. radial energy transport (ignoring VT)
10. ion charge exchange
11. neutral shielding (thermals and Franck-Condons)
12. finite beta

A large number of cases have been investigated, and a representative sample are described below. For each case considered, the microwave power is varied from 1 watt to 10^6 watts. Convergence is obtained only if a reasonably close initial trial solution is supplied. This was usually done by using SIMULT with constant field and low power to approach a steady state. Initial trial solutions for successively higher power levels are determined by fitting a quadratic curve to the preceding three solutions for each unknown. In spite of this, convergence usually fails before the power reaches 10^6 watts. It should also be pointed out that other solutions may exist depending on the time history of the approach to a steady state.

Small octupole: The terms used to describe confinement in the small octupole are identical to those used in the refined version of SIMULT. (In fact, the function statements can be directly transferred from one program to the other.) The parameters used are as follows: $T_{wall} = 0.025$ eV (room temperature), $L = 270$ cm (major circumference of toroid), $a = 18$ cm (adjusted so $\pi a^2 L = \text{total volume}$), A_0 (obstacle area) = 90 cm^2 (empirically determined from lifetime vs energy for ions and electrons), $p = 1 \times 10^{-5}$ torr (at plasma boundary assumed H_2), $B = 1$ kG (crude volume average), $f = 2.45$ GHz, and $Q = 2000$ (without plasma). The results shown in Fig. 1 agree remarkably well with both experimental results and with the peak values of the time-dependent program SIMULT. The results agree within 1 part in 10^6 with the steady state ($B = \text{constant}$) infinite time limit of SIMULT. The electron temperature stays nearly constant

at ~ 5 eV while the density increases linearly with microwave power. The computer printout for this case is included in the appendix.

Large octupole: For the large octupole, the parameters were changed to the following: $L = 800$ cm, $a = 50$ cm, $A_0 = 700$ cm 2 (actual geometric surface area of levators), $p = 1 \times 10^{-6}$ torr, $B = 1$ kG, $f = 2.45$ GHz, and $Q = 20,000$. The results shown in Fig. 2 are similar to those for the small octupole and agree almost perfectly with published values (Fig. 5 of Phys. Fluids 14, 1795 (1971)). With levitation ($A_0 = 0$), Fig. 3 shows that the electron temperature is lower and the density is higher, but this case is probably unrealistic because with classical radial diffusion as the only particle loss mechanism, the time required to reach a steady state is much longer than the duration of the magnetic field pulse. For this case, the time dependent program SIMULT would be more appropriate. One use for this program would be to try various loss terms with different parametric dependences, seeking a good fit between the density vs microwave power curve and experimental measurements. In this way some information about the nature of the anomalous losses in levitated multipoles can hopefully be obtained.

Toroidal quadrupole: The Wisconsin toroidal quadrupole (without ohmic heating) was investigated using the following parameters: $T_{\text{wall}} = 0.025$ eV, $L = 160$ cm, $a = 6$ cm, $A_0 = 3$ cm 2 , $p = 1 \times 10^{-4}$ torr, $B = 1$ kG, $f = 3$ GHz, and $Q = 500$. The results are shown in Fig. 4. The electron temperature is nearly constant at 3 eV and

the density increases linearly with microwave power. The actual density in the experiment is considerably below the predicted value at 10 kW input power, and this is evidence either of anomalous losses (perhaps instabilities) or of the absence of a steady state (unlikely), or of a high reflected microwave power (very likely).

UWFCE mirror: The electron cyclotron heated mirror device in B442 Engineering was studied by adding a loss cone term as described in PLP 518. The term includes scattering of electrons and ions on one another as well as on neutrals. Ambipolar potentials are also considered. The parameters are as follows: $T_{\text{wall}} = 0.025 \text{ eV}$, $L = 60 \text{ cm}$, $a = 6 \text{ cm}$ (limiter radius), $A_0 = 0$, $p = 1 \times 10^{-4} \text{ torr}$, $B = 1 \text{ kG}$, $f = 2.45 \text{ GHz}$, and $Q = 500$. Figure 5 shows that T_e stays nearly constant at $\sim 30 \text{ eV}$ while the density increases linearly with power in reasonable agreement with experiment. In the experiment there is also a runaway component of electrons ($> 10 \text{ keV}$) not treated in the calculation. These energetic electrons have only a small effect on the particle and power balance, however.

ELMO mirror: The Oak Ridge ELMO mirror device was treated in the same way as above using the following parameters: $T_{\text{wall}} = 0.025 \text{ eV}$, $L = 25 \text{ cm}$, $a = 10 \text{ cm}$, $A_0 = 0$, $p = 5 \times 10^{-5} \text{ torr}$, $B = 3 \text{ kG}$, $f = 10.6 \text{ GHz}$, and $Q = 10,000$. The results shown in Fig. 6 are very similar to those in Fig. 5, but differ by as much as an order of magnitude from those predicted by the less refined Oak Ridge program SIMULEBT (PLP 489).

ELMO Bumpy Torus: The Oak Ridge ELMO Bumpy Torus was studied using the following parameters: $T_{\text{wall}} = 0.025 \text{ eV}$, $a = 10 \text{ cm}$, $L = 175 \text{ cm}$, $A_0 = 0$, $p = 1 \times 10^{-5} \text{ torr}$, $B = 5 \text{ kG}$, $f = 18 \text{ GHz}$, and $Q = 10,000$.

A neoclassical radial diffusion term as proposed by Guest (ORNL-TM-3694) was used. Ambipolar potentials were neglected, and ions were assumed to diffuse at the same rate as electrons (as suggested by Guest). Electron-neutral collisions were added, however, and the radial energy transport corresponding to this particle diffusion (ignoring VT) was taken from Kovrzhnykh (Sov. Phys. - JETP 29, 475 (1969)). The results shown in Fig. 7 give a somewhat higher density and lower temperature than was previously calculated using SIMULEBT (PLP 489). It has not been possible to get numerical convergence for powers above 1 kW, and so the interesting collisionless regime which the experiment will hopefully reach (with powers \sim 30 kW) has not been investigated. The EBT case was also run with Bohm diffusion, and the result is shown in Fig. 8. There is not a great difference from the neoclassical case, as has been pointed out before (ORNL-TM-3694). Experimental measurements should be forthcoming.


```

ULP(IPw)=ANALOG1(XFIN(1))+1.0
TEP(IPw)=ANALOG1(XFIN(2))+1.0
TIP(IPw)=ANALOG1(XFIN(3))+1.0
UNP(IPw)=ANALOG1(XFIN(4))+1.0
DO 700 I=1,4
IF (IPw.EQ.1) XINIT(I)=XFIN(I)
IF (IPw.EQ.2) XINIT(I)=XFIN(I)**2/XOLD(I)
IF (IPw.EQ.3) XINIT(I)=SQRT(XOLD2(I)*XFIN(I)**2)/XOLD(I)**2
IF (IPw.EQ.2) XOLD2(I)=XOLD(I)
XOLD(I)=XFIN(I)
IPw=IPw+1
IF (IPw.LE.31) GO TO 200
900 CONTINUE

```

C GRAPH OUTPUT

```

IPw=IPw-1
CALL GRPHA(PP,IR1,LEP,PK,IPw,'x6111',ONE,ZERO,S TIME INDEPENDENT
SINGLE SIMULATION.'MICROWAVE POWER...INTENSITY AND TEMP...',IT)
CALL GRPHzV(PP,IR1,TEP,PK,IPw,'NONE',IT)
CALL GRPHzV(PP,IR1,TIP,PK,IPw,'NONE',IT)
CALL GRPHzV(PP,IR1,UNP,PK,IPw,'NONE',IT)
CALL GRPHND
STOP
END

```

COMPILE TIME: NO - DIAGNOSTICS.

```

C
• 205-16/12/73-09:06:56          AUXFCN
AUXFCN(X,T)
FUNCTION AUXFCN(X,T)
DIMENSION X(1)
COMMON P,TWALL,TVAL,AL,RES,BUFFER
C
C      DEFINE FUNCTIONS - OC,UPOLE
C      D1 IS D/DT DUE TO IONIZATION
C      D1(DENS,DNEUT,TE)=571.0*DENS*DNEUT*SQRT(TE)*EXP(-15.0/TE)*(TE/(20.
C      20*TE+15.0)+ALOG(1.5625+.1*TE))/(TE+15.0)
C      D2 IS D/DT DUE TO DIFFUSION
C      D2(DENS,TE)=DENS*(0.33*DENS/SQRT(TE)+0.601*DNEUT*TE)/B/B/A/A
C      D3 IS D/DT DUE TO OBSTACLE LOSSES
C      D3(DENS,TE)=2.0*50*DENS*.0*SQRT(TE+TIA)/A/A/L
C      D4 IS D/DT DUE TO FIELD DECAY
C      D4(DENS)=0.5*D2*(A/A/L-5)/60*L/DT
C      PE1 IS QDE/DT DUE TO MICROWAVES
C      PE1(P)=1.0E9*P*EA/(DEA+DEG)/A/A/L
C      PE2 IS QDE/DT DUE TO IO. COLLISIONS
C      PE2(DENS,TE,TI)=2.0*DENS**2*(1E-TI)*ALO.(5.2E11*TE**3/ABS(LENS)
C      2/(40.0+TE))/1E*1.5
C      PEO IS QDE/DT DUE TO EXCITATION
C      PEO(DENS,DNEUT,TE)=29.1*D1(DENS,DNEUT,TE)*EXP(6.98/(TE+0.1))
C      PE4 IS QDE/DT DUE TO BREMSSTRANSLONG
C      PE4(DENS,TE)=1.0E-4*DENS*DENS*SQRT(TE)
C      PEO IS QDE/DT DUE TO SYNCHROTRON RADIATION
C      PEO(DEA,TE)=3.7E-3*DENS*8*B*TE*(1.0+TE/2.0*DEG)
C      PEO IS QDE/DT DUE TO THERMAL CONDUCTION
C      PEO(DENS,TE)=(2.5*D2(DEA,TE)+2.0*D3(DEA,TE)+D4(DEA))*(TE-TWALL)
C      P10 IS QD1/DT DUE TO CHARGE EXCHANGE
C      P10(DENS,DNEUT,TE)=6.01*6*DENS*DNEUT*TE*(TI-TWALL)/(TI+100.0)
C      P10 IS QD1/DT DUE TO THERMAL CONDUCTION
C      P10(DENS,TE,TI)=(2.5*D2(DEA,TE)+2.0*D3(DEA,TE)+D4(DEA))*(TI-TWALL)
C
DEA=X(1)
DENS=DEA/
TEA=X(2)
IF(TEA.LT.20.0*TWALL)TEA=20*TWALL*ALOG(EXP(4.*TEA/TWALL)+1.0)+.01)
TE=TEA
TIA=X(3)
IF(TIA.LT.20.0*TWALL)TIA=20*TWALL*ALOG(EXP(4.0*TIA/TWALL)+1.0)
TI=TI
DNEUT=X(4)
SF=SQRT(.35*(50*DEA+.05*DEA**2)*DEA*(TEA+TIA)))
GOLDFB
BT=1.0
GO TO (1,2,3,4),R
CONTINUE
AUXFCN=(D1(DEA,DNEUT,TE)-D2(DEA,TEA)-D3(DEA,TEA)-D4(DEA))/DENS
RETURN
CONTINU
DEOF=F+F*(3.0045+(F/F)**2+123.0*(B/F)**2+0.006677)/F
AUXFCN=(PL1(P)-PE2(DEA,TEA,TIA)-PL3(DEA,DNEUT,TEA)-PE4(DEA,TEA)
-EPE5(DEA,TEA)-P10(DEA,TEA))/DENS
RETURN
CONTINU

```

```
AUXFCN=(P22(DEA,TEA,TIA)+P13(DEA,DNEUT,TIA)+P16(DEA,TEA,TIA))/DENS
```

```
RETURN
```

```
CONTINUE
```

```
DNF=322.0*PRES*XP(-1.2E-0*A*B1(DEA,DNEUT,TEA)/DNEUT)
```

```
DNF=120.0*PRES*XP(-6.9E-0*A*B1(DEA,DNEUT,TEA)/DNEUT)
```

```
AUXFCN=DNEUT-DNF-DNF
```

```
RETURN
```

```
END
```

COMPILETIME: NO DIAGNOSTICS.

RESULTS TERM

TE POWER

INITIAL

F1B

U3 T

U4

U5

U6

U7

U8

U9

U10

U11

U12

U13

U14

U15

U16

U17

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RunID: C6J_5B REQUEST: 3_700

ITEM

ITEM	PRICE	COST(USLARS)
CPU UNIT	0.0200:0.5•0.14	\$0.31
1/2 READER/2 1/2 WORK STAND-ERKLE	220.20	\$0.24
CORE USLAR	0.151	\$0.11
CARDS 1,	0.43	\$0.07
PAGES P1 UNIT	0	\$0.04
DDU UNIT	4	\$0.05
TOTAL COST		\$0.90

THE ABOVE BILLING ACCOUNTS ARE APPROXIMATE AND ARE BASED ON RATES FOR WRITE-OUT

DETERMINATION TIME:

09:06:44-05/11/12, 1973

TERMINATION TIME:

09:07:06-05/11/12, 1973

PREVIOUS RUN TIME:

09:07:41-05/11/12, 1973

ZERO- τ TIME INDEPENDENT SIMULATION

DENSITY AND THERM

	0.000	1.000	2.000	3.000	4.000	5.000	6.000
0.000	+	+	+	+	+	+	+
+1	+	+	+	+	N	N	N
+1	+	+	+	+	N	N	N
+1	L	D	L	N	N	N	N
+1	D	D	E	N	N	N	N
+1	D	E	N	N	N	N	N
+1	D	E	N	N	N	N	N
1.000	+	+	+	+	N	N	N
+	+	+	+	+	N	N	N
+	I	E	I	N	N	N	N
+	I	E	D	N	N	N	N
+	I	E	D	N	N	N	N
+	I	E	D	N	N	N	N
+	I	E	D	N	N	N	N
2.000	+	+	+	+	D	D	D
+	+	+	+	+	D	D	D
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
3.000	+	+	+	+	D	D	D
+	+	+	+	+	D	D	D
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
+	I	E	I	N	N	N	N
4.000	+	+	+	+	N	D	D
+	+	+	+	+	N	D	D
+	I	E	I	N	N	D	D
+	I	E	I	N	N	D	D
+	I	E	I	N	N	D	D
5.000	+	+	+	+	N	D	D
+	+	+	+	+	N	D	D
+	I	E	I	N	N	D	D
+	I	E	I	N	N	D	D
+	I	E	I	N	N	D	D
6.000	+	+	+	+	+	+	+
+	+	+	+	+	+	+	+
+	I	E	I	N	N	+	+
+	I	E	I	N	N	+	+
+	I	E	I	N	N	+	+

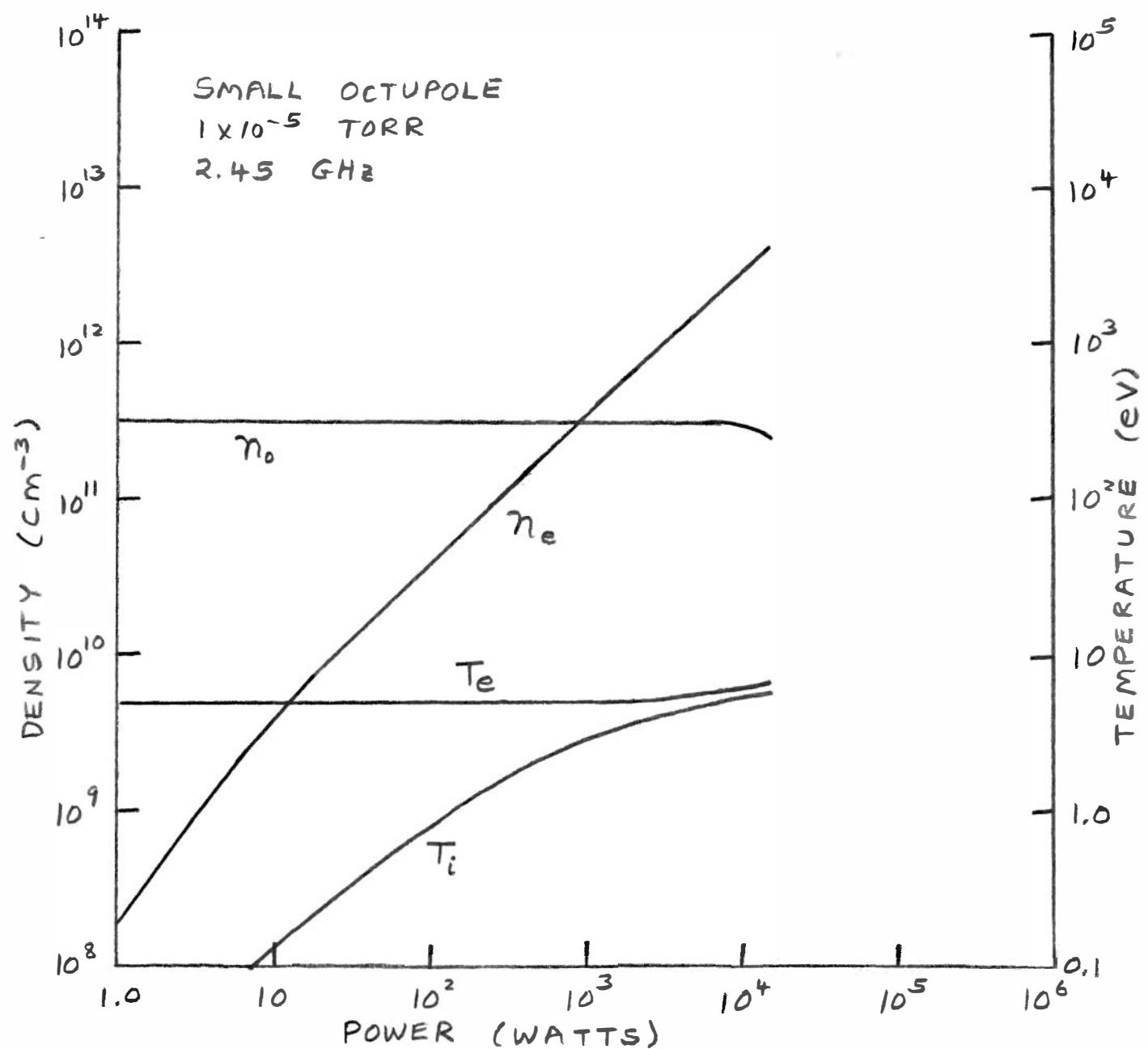


FIG 1

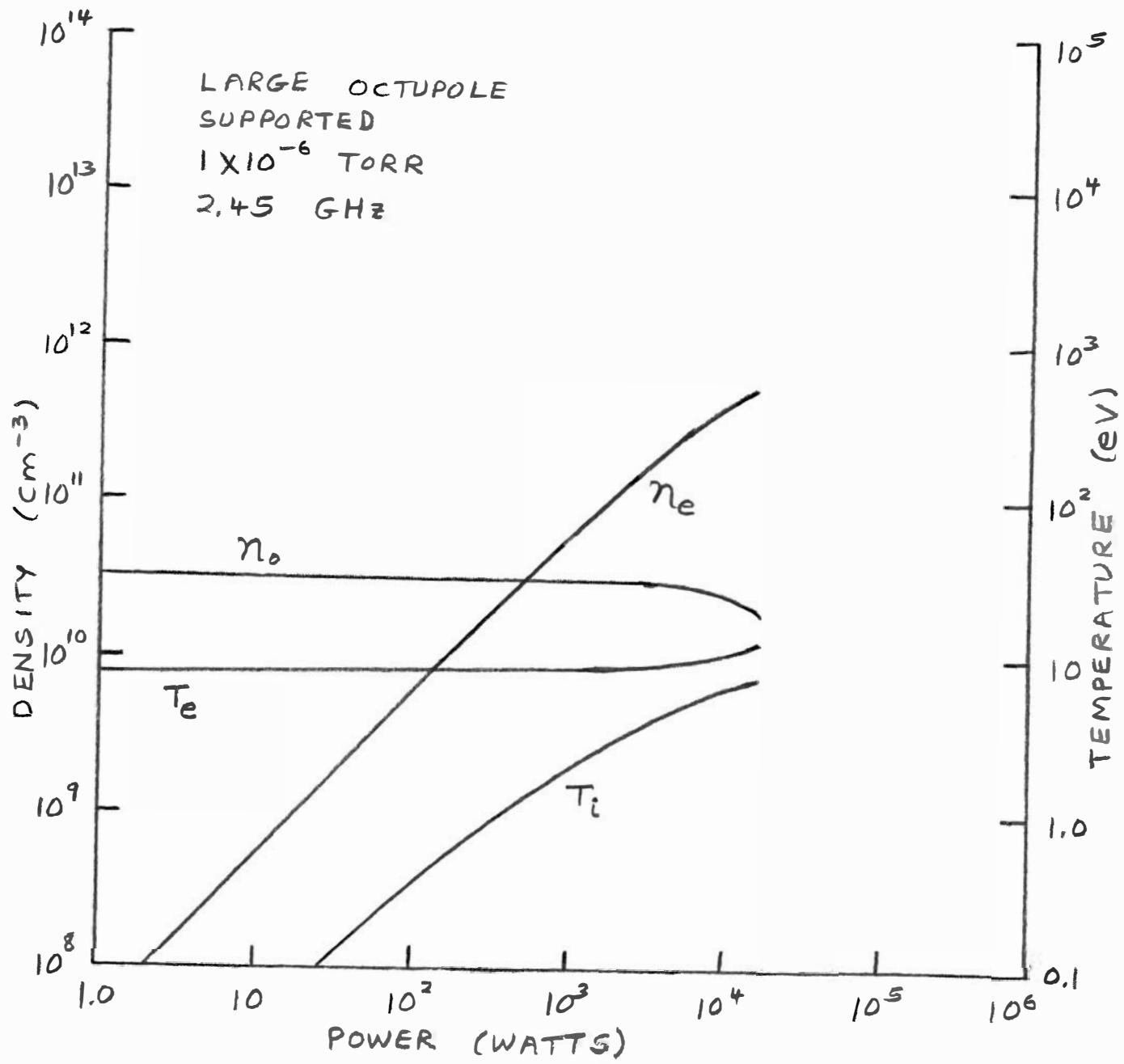


FIG 2

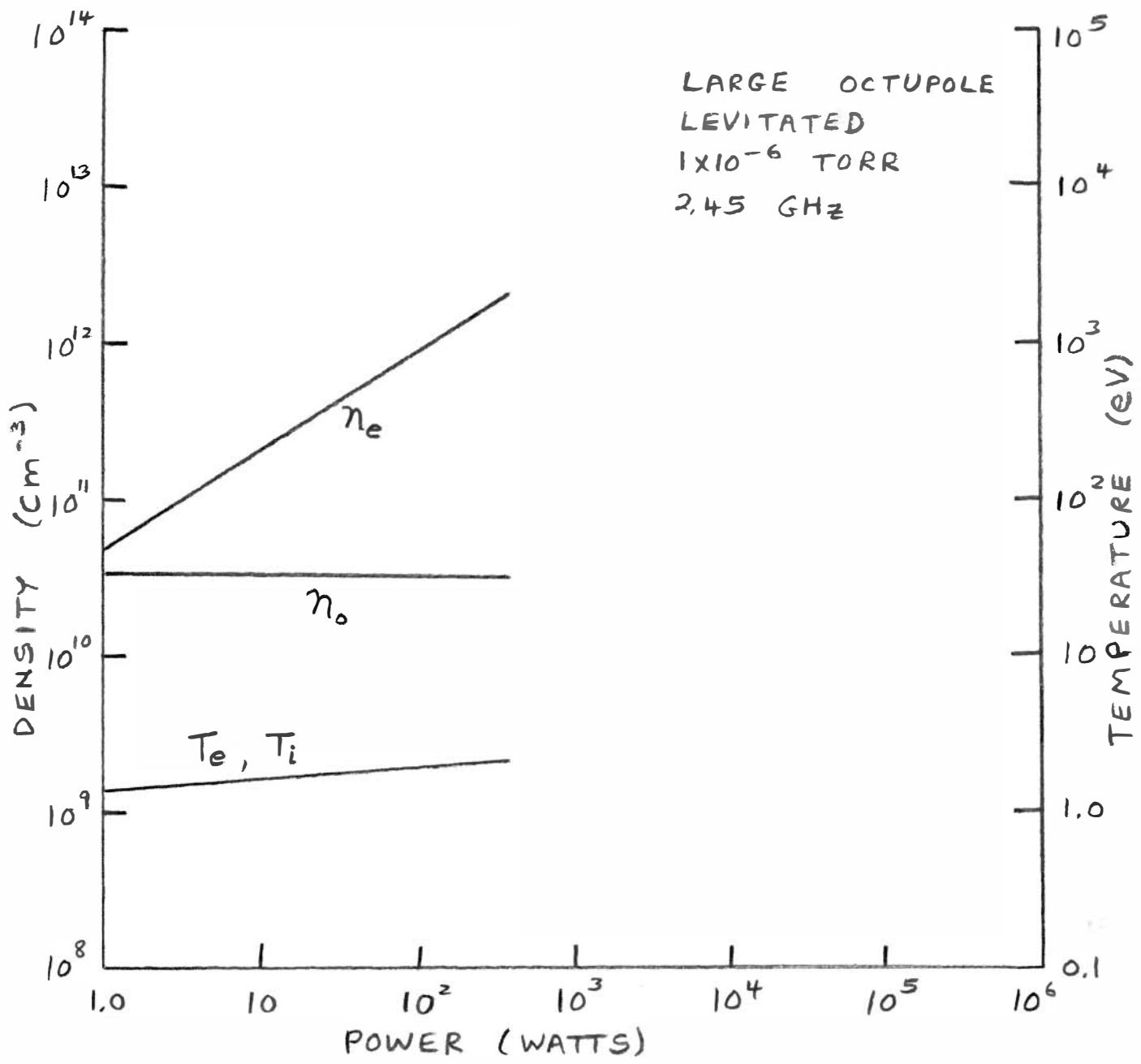


FIG 3

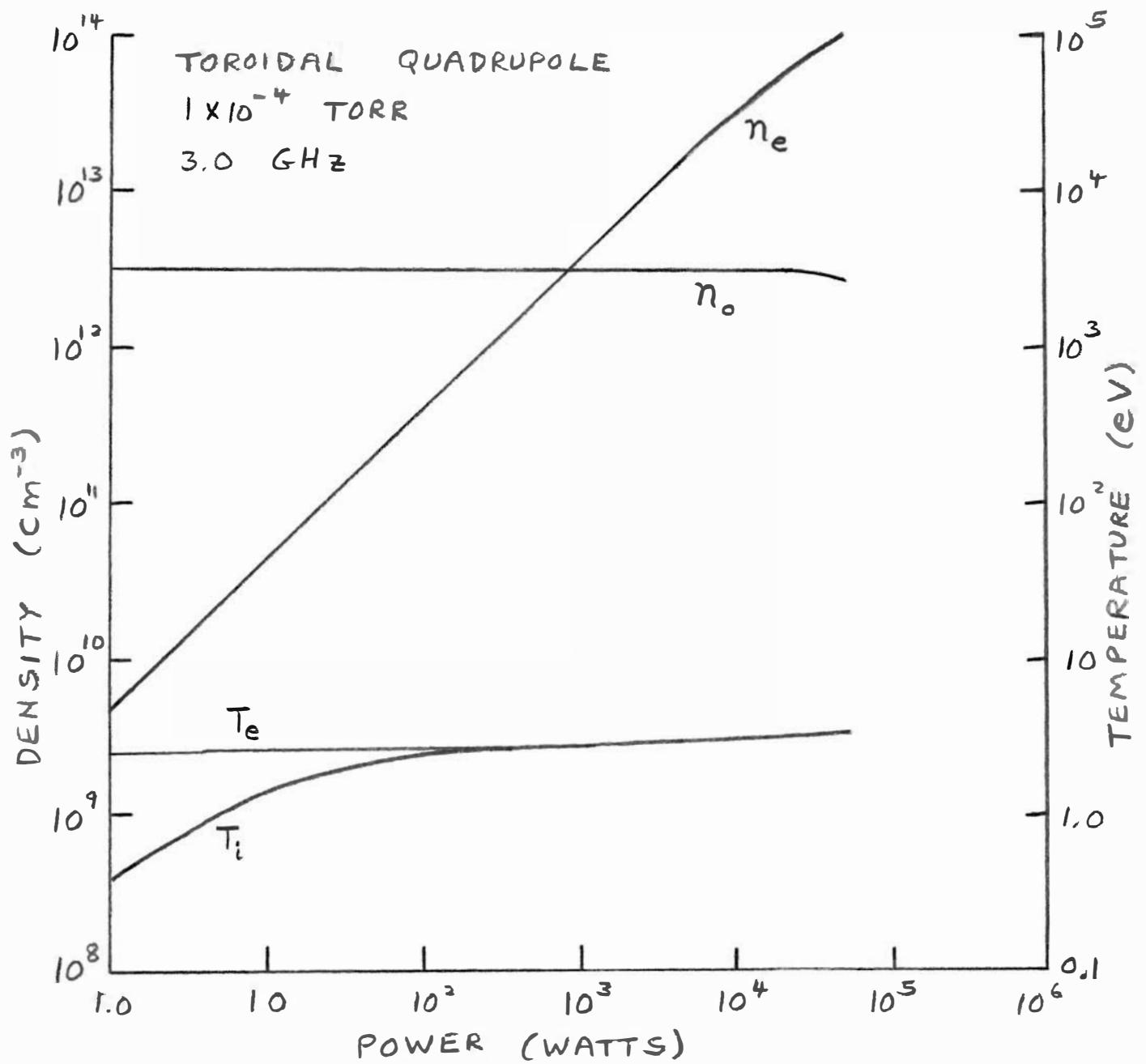


FIG 4

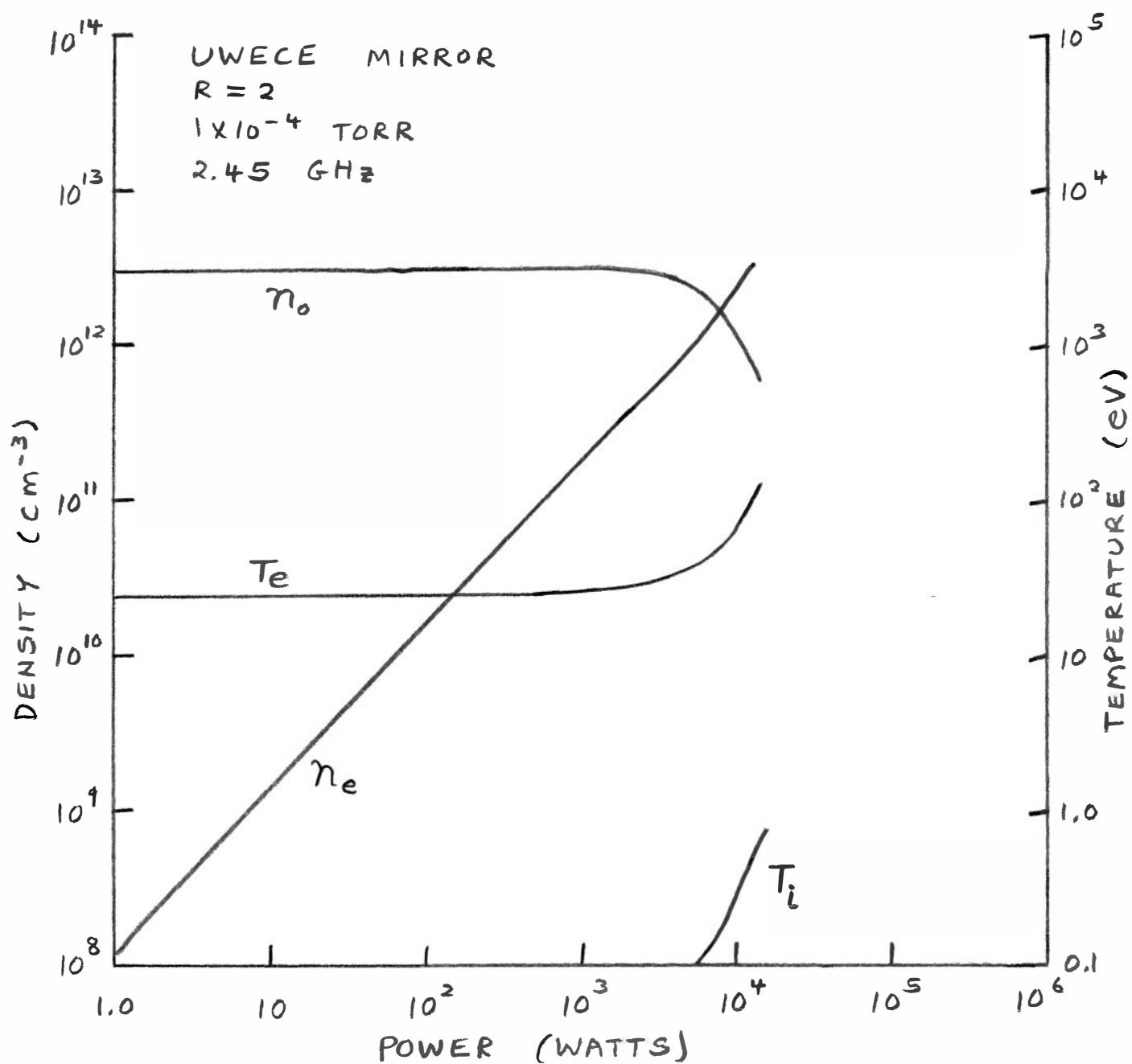


FIG 5

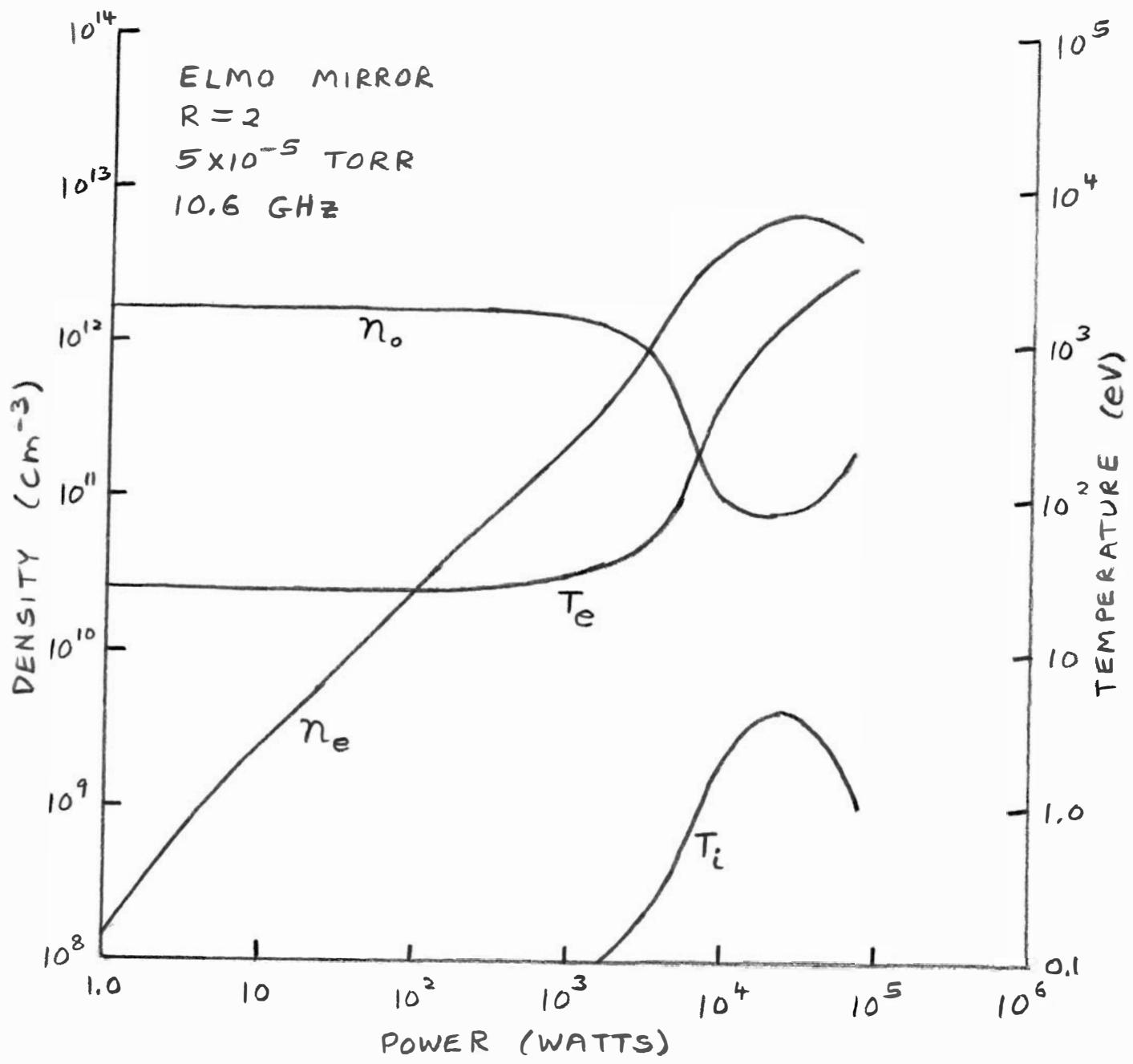


FIG 6

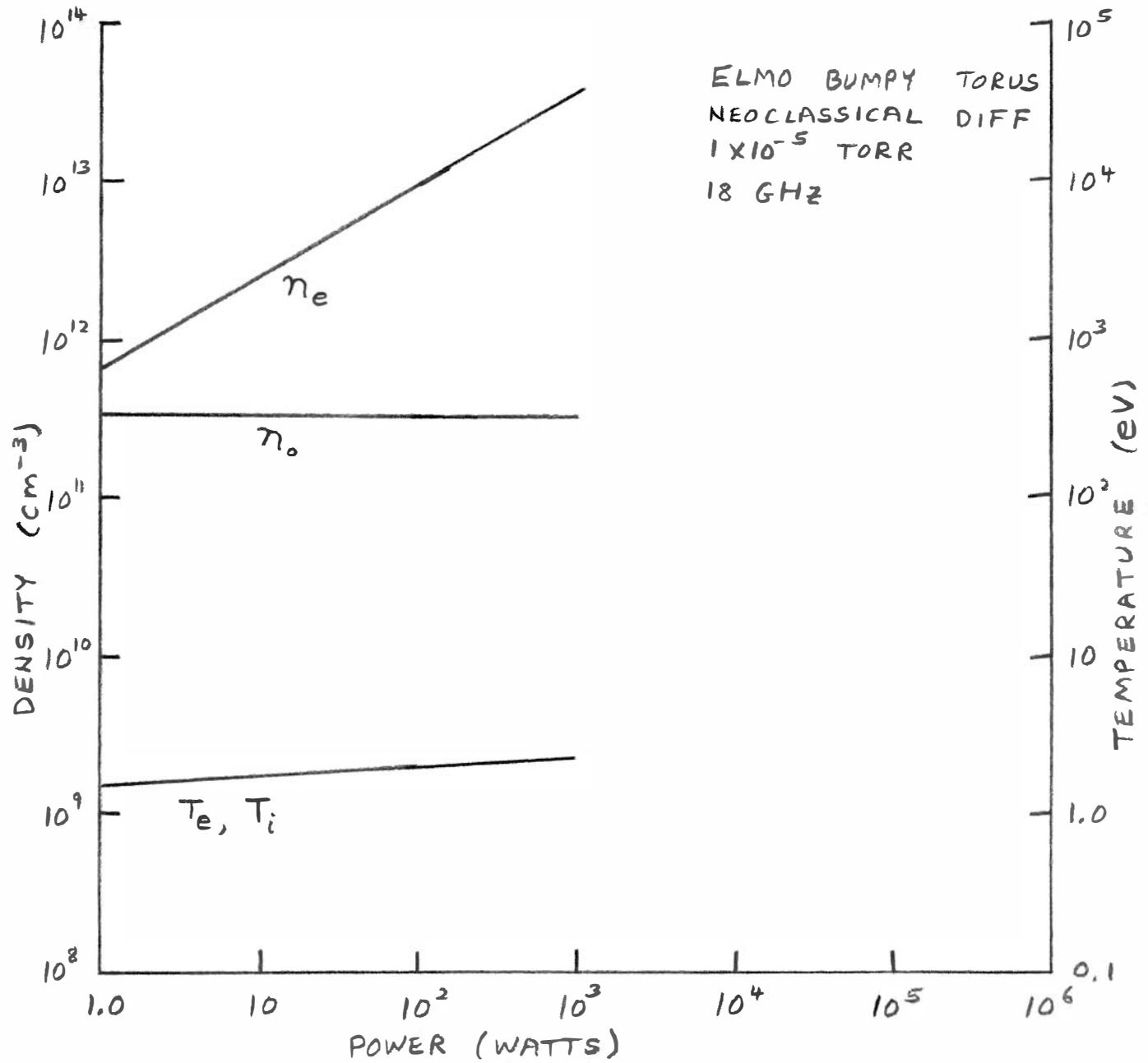


FIG 7

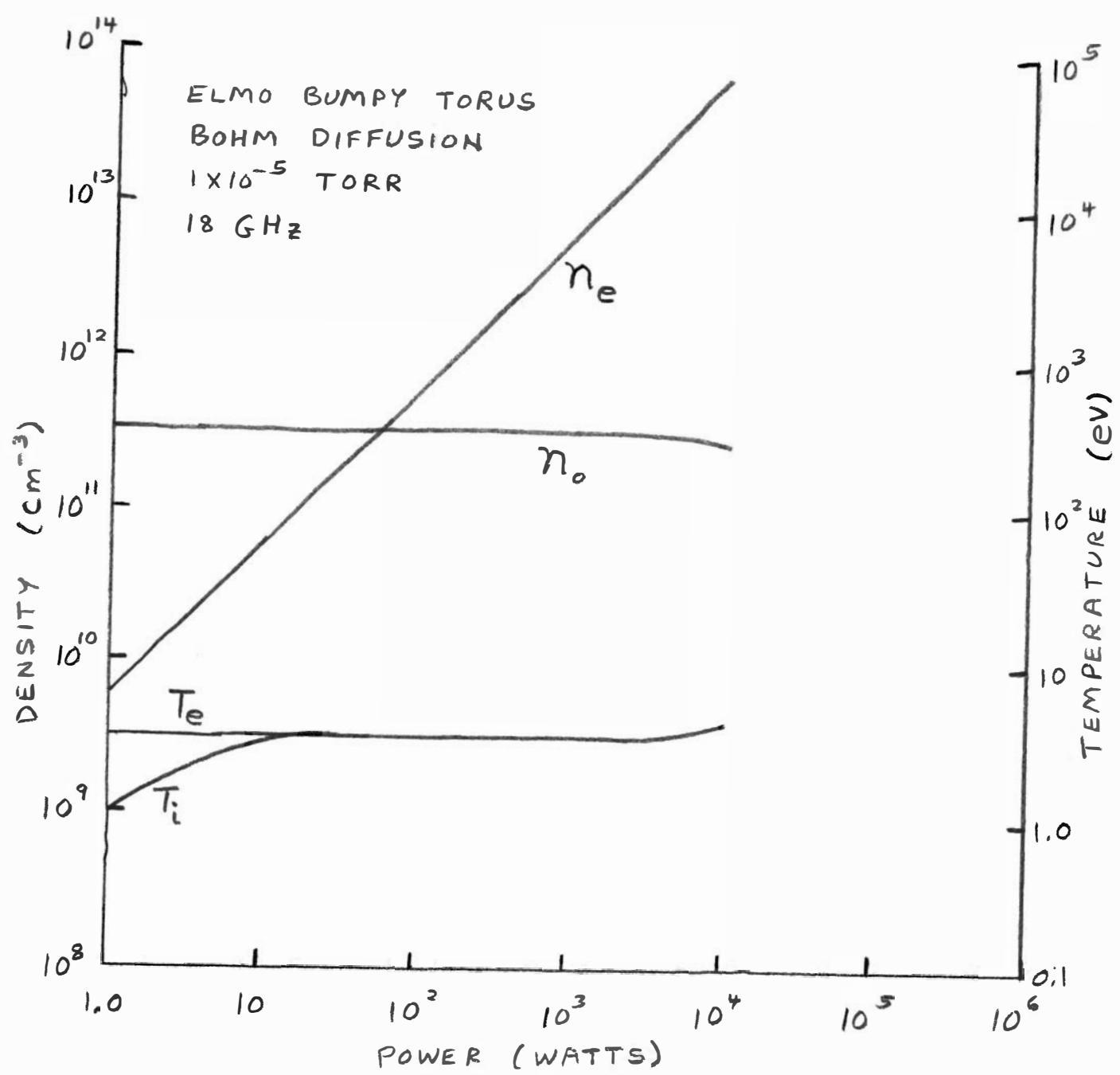


FIG 8